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 ACCESSION NUMBER: 1999(7):28243 ENERGY
 TITLE: Reduction and reoxidation of cobalt Fischer-Tropsch catalysts.
 AUTHOR: Hilmen, Anne-Mette
 CORPORATE SOURCE: Norges teknisk-naturvitenskapelige univ., Trondheim (Norway)
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 DOCUMENT TYPE: Report; Dissertation
 COUNTRY: Norway
 LANGUAGE: English
 FIELD AVAILABILITY: AB
 ABSTRACT: The Fischer-Tropsch synthesis involves the hydrogenation of carbon monoxide to produce mainly hydrocarbons, water and carbon dioxide, but also alcohols, aldehydes and acids are formed. The distribution of these products is determined by the choice of catalyst and synthesis conditions. This thesis studies the reduction and reoxidation of 17%Co/Al₂O₃ and 17%Co-1%Re/Al₂O₃ by means of several characterization techniques. The effect of small amounts of Re on the reduction properties of Al₂O₃-supported Co catalysts has been studied by temperature-programmed reduction (TPR). An intimate mixture of Co/Al₂O₃ and Re/Al₂O₃ catalysts showed a promoting effect of Re similar to that for co impregnated CoRe/Al₂O₃. A loose mixture of Co/Al₂O₃ + Re/Al₂O₃ did not show any effect of Re on the reduction of Co. But a promoting effect was observed if the mixture had been pre-treated with Ar saturated with water before the TPR. It is suggested that Re promotes the reduction of Co oxide by hydrogen spillover. It is shown that a high temperature TPR peak at 1200K assigned to Co aluminate is mainly caused by the diffusion of Co ions during the TPR and not during calcination. The Co particle size measured by x-ray diffraction on oxidized catalysts decreased compared to the particle size on the calcined catalysts, while the dispersion measured by volumetric chemisorption decreased somewhat after the oxidation-reduction treatment. The role of water in the deactivation of Co/Al₂O₃ and CoRe/Al₂O₃ Fischer-Tropsch catalysts has been extensively studied. There were significant differences in the reducibility of the phases formed for the two catalysts during exposure to H₂O/He. 113 refs., 76 figs., 18 tabs.
 CLASSIFICATION CODE: *010408
 CONTROLLED TERM: ALCOHOLS; ALDEHYDES; CARBON DIOXIDE; CARBON MONOXIDE; CATALYSTS; CHEMICAL REACTIONS; FISCHER-TROPSCH SYNTHESIS; HYDROCARBONS; HYDROGENATION; NATURAL GAS; REDUCTION
 BROADER TERM: CARBON COMPOUNDS; CARBON OXIDES; CHALCOGENIDES; CHEMICAL REACTIONS; ENERGY SOURCES; FLUIDS; FOSSIL FUELS; FUEL GAS; FUELS; GAS FUELS; GASES; HYDROXY COMPOUNDS; ORGANIC COMPOUNDS; OXIDES; OXYGEN COMPOUNDS
 ELEMENT TERM: Co; Al*O; Al₂O₃; Al cp; cp; O cp; Co*Re; Co sy 2; sy 2; Re sy 2; Co-1%Re; Re; Al*Co*O; Al sy 3; sy 3; Co sy 3; O sy 3; CoAl₂O₃; Co cp; CoRe; Re cp; Ar; K; H*O;

H₂O; H cp

PATENT APPLICATION

ACCESSION NUMBER: 325446 EUROPATFULL EW 198930 FS OS STA B
 TITLE: Impurity removal from carbon monoxide and/or hydrogen-containing streams.
 INVENTOR(S): Butler, Gerald Eugene c/o EASTMAN KODAK COMPANY, Patent Department 343 State Street, Rochester New York 14650, US
 PATENT ASSIGNEE(S): EASTMAN KODAK COMPANY, 343 State Street, Rochester New York 14650, US
 PATENT ASSIGNEE NO: 201211
 AGENT: Davis, Ian Ellison et al, Kodak Limited Patent Department Headstone Drive, Harrow Middlesex HA1 4TY, GB
 AGENT NUMBER: 29961
 OTHER SOURCE: ESP1989031 EP 0325446 A2 890726
 SOURCE: Wila-EPZ-1989-H30-T1
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'OFFENLEGUNGS' DATE:		19890726
APPLICATION INFO.:	EP 1989-300484	19890119
PRIORITY APPLN. INFO.:	US 1988-146756	19880122
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ABSTRACT (ENGLISH):

Disclosed is a process for the purification of carbon monoxide and/or hydrogen-containing gas streams employed for chemical conversion reactions by contacting such gas feed streams with the oxygenated organic reaction products obtained in the subject chemical conversion reaction.

DESCRIPTION (ENGLISH):

This invention relates to the purification of gas feed streams comprising carbon monoxide and/or hydrogen. In a particular aspect, this invention relates to an integrated process wherein the reaction product stream is employed to purify the feed gases employed for a chemical conversion process.

Background of the Invention

Many chemical conversions are known which employ hydrogen and/or carbon monoxide-containing gases. These gases frequently contain small amounts of impurities which are detrimental to the desired chemical conversions. As a result, numerous treat.shy. ments have been developed to remove such impurities such as oxygen, elemental sulfur, organic as well as inorganic sulfur compounds, iron, and the like. Each such impurity removal process introduces added requirements for equipment (e.g., scrubbers, guard beds, and the like), the maintenance thereof, utility consumption, and the like. It would be desirable to eliminate the need for such added equipment and materials as fixed beds containing alumni, zinc oxide, and the like.

Accordingly, a relatively simple, inexpensive means to remove undesirable

impurities from carbon monoxide and/or hydrogen-containing feed streams would be of great benefit to numerous chemical conversion reactions.

Objects of the Invention

An object of the present invention, therefore, is a process for the removal of impurities from carbon monoxide and/or hydrogen-containing feed streams employed for chemical conversion reactions.

Another object of the present invention is a chemical conversion process employing carbon monoxide and/or hydrogen-containing gases wherein **deactivating** impurities are readily and inexpensively removed from the gaseous feed stream.

These and other objects of the present invention will become apparent upon inspection of the detailed description and appended claims which follow.

Statement of the Invention

In accordance with the present invention, I have discovered that the common impurities in carbon monoxide and/or hydrogen-containing feed streams, i.e., oxygen, sulfur, iron, and the like, can be removed by contacting such gas streams with the oxygenated product stream obtained from a process in which the carbon monoxide and/or hydrogen are fed as a co-reactant.

The practice of the present invention allows one to eliminate the need for ancillary gas purification equipment, such as a fixed bed purification column, thereby saving the capital and maintenance costs associated with such equipment. In addition, the invention process enables the efficient recovery and recycle of unreacted gaseous components from the product stream. Moreover, the invention process accomplishes the removal of many undesirable components from the carbon monoxide and/or hydrogen-containing feed streams, including water vapor.

Brief Description of the Figure

Figure 1 is a flow diagram of an exemplary scheme incorporating the process of the present invention.

Detailed Description of the Invention

In accordance with the present invention, there is provided a process for purifying a feed gas employed in a chemical conversion process for the production of oxygenated compounds, wherein the feed gas comprises carbon monoxide and/or hydrogen. The invention process comprises intimately contacting the feed gas with at least a portion of the oxygenated product stream obtained from the chemical conversion process prior to introducing the feed gas into the chemical conversion reaction zone. The invention process is applicable to such conversions as the hydroformylation reaction, the Fisher-Tropsch reaction, homologation reaction, anhydride-forming reactions, and the like.

The contacting of feed gas with oxygenated product stream in accordance with the present invention can be carried out under a variety of conditions. For example, the pressure of the contacting can vary from about 7 up to 40 atmospheres. Preferably, pressure of the contacting will be carried out at approximately the same pressure as is being employed for the chemical conversion process. In this way, unreacted feed components for the desired conversion can be stripped from the crude oxygenated product and recycled into the chemical conversion reaction without the need for recompression, cooling, condensation, or the like.

Similarly, the temperature at which the contacting is performed can vary widely, and will be a function of the pressure, the nature of the oxygenated product employed for the contacting, the length of time during which feed gas and oxygenated product are maintained in intimate contact, and the like. The lower temperature employed is determined by the efficiency of impurity removal desired (with contacting at too low a temperature being essentially ineffectual); while at excessively high contact temperatures, substantial quantities of liquid reaction product are stripped from Vessel 11 and returned to the reactor. In addition, excessively high temperatures cause an increased formation of by-products. Typically, temperatures in the range of about 25.degree. up to 100.degree.C are suitable for the contacting, with temperatures in the range of about 40.degree. up to 65.degree.C being preferred.

The contacting time and ratio of feed gas to liquid oxygenated reaction product can each vary widely. Generally, sufficient time of contact is maintained to allow a major proportion of the feed gas impurities to be absorbed by the liquid reaction product. Similarly most any ratio of feed gas to liquid is suitable, so long as the volume of liquid employed is sufficient to absorb a major proportion of the impurities contained in the feed gas.

Referring now to Figure 1, the invention will be described with particular reference to the apparatus illustrated therein. The flow of crude feed gases via Line 1 and recycled gases via Line 53 into Compressor 7 is controlled by Valve 3. The combined gas stream is subjected to compression up to the desired reaction pressure then passed through Line 9 into Vessel 11 in which the crude feed gas stream and a portion of reactor effluent are brought into intimate contact with one another.

As employed in this specification, the term "intimate contact" refers to any means by which the gas-liquid interface between crude feed gas and reactor effluent is maximized. Those of skill in the art recognize that this can be accomplished in a variety of ways. For example, the crude feed gas can be passed upwardly in a countercurrent fashion through a body of reactor effluent. Alternatively, crude feed gas can be sparged into a body of reactor effluent. The column dimensions can vary widely and are not believed to be critical. The presence of column packings may increase the efficiency of the contacting operation, as will certain column designs which cause turbulent fluid flow through the column to occur.

Once crude feed gases and reaction product have been intimately contacted, the treated feed gas stream passes via Line 13 and is combined with organic feed stream (introduced via Line 17), with the combined feed streams being introduced into Reactor 19 (via Line 15). After having contacted crude feed gas in Vessel 11, crude oxygenated reaction product is removed from Vessel 11 via Line 45 where product is recycled to Vessel 11 via Pump 57 and Line 59 (in order to control the gas/liquid ratio), or product is controllably delivered to Flash Tank 51 via Valve 47 and Line 49. The gases obtained in the flash tank are recycled via Line 53 and admixed with additional crude feed gas being introduced via Line 1. The crude reaction product obtained from the crude reaction tank is removed via Line 55 and delivered to crude product tank for further manipulation.

Returning now to Reactor 19, reactor volume is maintained fairly constant by removing a vaporous stream overhead via Line 21. The vaporous reactor effluent is passed through Chiller 23 then into Vapor/Liquid Separator 27 via Line 25. Gaseous products are taken overhead via Line 29 and either recirculated to the reaction vessel via Line 33, Recirculator 35, Lines 37 and 15 or, as appropriate, overhead gases are removed from the reaction train via inert Purge Line 31. Liquid product is removed from Vapor/Liquid Separator 27 via Line 39. This material is then pumped via Pump 41 through Line 43 into Vessel 11 where the crude reaction product is contacted with additional quantities of crude feed gas.

As Figure 1 and the above description of the figure make clear, the oxygenated reaction product itself is used to remove undesirable impurities from the crude feed gas stream. At the same time, unreacted quantities of the organic reactant feed via Line 17 can be stripped from the crude product stream in Vessel 11 and returned directly to the reaction vessel (No. 19) without the need for recompression of such organic feed material.

Exemplary chemical conversion processes contemplated by the present invention include the hydroformylation reaction, the **Fischer-Tropsch** reaction, homologation reaction, anhydride-forming reactions, and the like. A presently preferred application of the invention process is in the hydroformylation reaction, wherein olefins having 2 up to 20 carbon atoms are converted to **aldehydes** having $n + 1$ carbon atoms. Preferred olefins are α -olefins having 2 up to 8 carbon atoms. Exemplary hydroformylation reactions include the conversion of propylene to n-butyraldehyde, ethylene to propionaldehyde, butenes to valeraldehydes, as well as conversions of mixed olefin feeds to produce mixed **aldehyde** products.

~~The invention will now be described in greater detail by reference to the following non-limiting examples.~~

Example 1: Effect of Temperature on Oxygen Removal

Example 1 shows how the process of the present invention can be employed to remove molecular oxygen from a crude synthesis gas stream using the product liquid of a hydroformylation reaction. A hydroformylation reaction utilizing a rhodium-phosphine catalyst system to produce butyraldehydes was operated at a pressure of 18 bars. The molecular oxygen scrubber employed was a 6-inch diameter by 12 foot tall tower packed with 1/2-inch stainless steel Pall rings. A ratio of product liquid to crude feed gas of 5.12 gal. of product liquid per standard cubic foot (std. ft.^{sup3.}) of feed gas was maintained, at a feed gas rate of about 187 std. ft.^{sup3.}/hour. When the average temperature of the molecular oxygen scrubber was about 40.degree.C, the average daily phosphine losses to phosphine oxide (caused by the presence of molecular oxygen in the feed gases) were 2.08 percent of the phosphine in the reactor. When the average temperature of the scrubber was increased to 55.degree.C, the average daily phosphine losses to phosphine oxide were reduced to 1.3875 percent of the phosphine in the reactor, for a 34 percent reduction in phosphine losses.

Example 2: Effect of Pressure on Oxygen Removal

An 8-inch diameter by 10-foot tall absorption tower filled with 3/4-inch Intalox saddles was used to evaluate absorption of trace quantities of oxygen from a stream of nitrogen using crude butyraldehydes as absorption liquid. In the first test the pressure of the system was 1 bar. An oxygen meter was used to measure oxygen concentration in both the incoming and outgoing nitrogen stream. In the second and third tests the pressure was raised to 7 bar. The temperature for all three tests was 50-60.degree.C.

The results are shown in Table 1. <table> The results indicate that 0.sub2 will be absorbed at both low pressure and high pressure but that oxygen absorption is more nearly complete at the higher pressure.

Example 3: Removal of Sulfur-Containing Impurities

A test was run to evaluate the removal of sulfur bearing lubricating oil from synthesis gas utilizing the scrubber described in Example 1. The lubricating oil contained 2,055 ppm sulfur. The addition of oil was at a

rate such that the sulfur content in the reactor would increase by 26 ppm per day if all the sulfur entered the reactor. During the 6 days of oil addition, the sulfur content in the reactor was unchanged. These data indicate the scrubber utilizing product **aldehydes** as absorption liquid will stop sulfur bearing oil from entering the reactor.

Example 4: Removal of Iron-Containing Impurities

A test was run to evaluate removal of iron carbonyl from synthesis gas utilizing the scrubber described in Example 1. A solution of iron-.shy. pentacarbonyl in butyraldehyde was added to the high pressure synthesis gas feed line between the compressor and the molecular oxygen scrubber. The scrubber temperature was 55.degree.C at the base. Scrubber pressure was about 19-bar. The iron containing solution was added continuously at a rate of about 0.04 gram of iron per hour for 72 hours. During this time a total of 0.024 gram iron accumulated in the reactor. This indicates that the scrubber removed 99.2 percent of the iron from the incoming synthesis gas.

Example 5: Recovery and Recycle of Unreacted Propylene From Crude Hydroformylation Product Stream

A test was run to evaluate desorption of low boilers from the crude product **aldehydes** using the apparatus described in Example 1. The crude product **aldehydes** were contacted at 14 bar and 55.degree.C with incoming synthesis gas. The crude **aldehydes** collected in Vessel 51 were then reduced in pressure to 0.5 bar and heated to 90.degree.C to force the dissolved low boilers to flash from the liquid to form a low pressure recycle stream.

In a comparison run, the crude product **aldehydes** were removed from the Reactor 19, passed directly to flash Chamber 27, then reduced in pressure from 14 bar to 0.5 bar, and heated to 90.degree.C to force dissolved synthesis gas and propylene to flash from the crude product **aldehydes**. These flashed gases make up the low pressure recycle.

The results of these runs are summarized in Table 2. <table> From Table 2 it is seen that the volume of low pressure recycle is very significantly reduced by contacting the crude product **aldehydes** with the incoming synthesis gas prior to letting down the pressure.

The invention has been described in detail with particular reference to preferred embodiments thereof, but it will be understood that variations and modifications can be effected without departure from the spirit and scope of the invention described and claimed.

CLAIMS (ENGLISH):

1. 1. A hydroformylation process for the conversion of olefins to oxygenated compounds comprising intimately contacting the carbon monoxide and hydrogen feed with at least a portion of the oxygenated product stream obtained from said hydroformylation reaction prior to introducing said carbon monoxide and hydrogen feed into the hydroformylation reaction zone.

2. 2. A process in accordance with Claim 1 wherein said intimate contacting is a countercurrent contacting of liquid oxygenated product stream and gaseous carbon monoxide and hydrogen feed.

3. 3. A process in accordance with Claim 2 wherein said countercurrent contacting is carried out at substantially the same pressure as is the hydroformylation process.

4. 4. A process in accordance with Claim 1 wherein said contacting is carried out at a temperature in the range of about 25.degree. up to

100.degree.C.

5. 5. A process in accordance with Claim 4 wherein said contacting is carried out at a temperature in the range of about 40.degree. up to 65.degree.C.

6. 6. A process in accordance with Claim 1 wherein said olefin converted in said hydroformylation process has in the range of 2 up to 8 carbon atoms.

7. 7. A process in accordance with Claim 2 wherein said olefin converted in said hydroformylation process is propylene and said oxygenated product stream comprises butyraldehyde.

8. 8. A process in accordance with Claim 2 wherein said olefin converted in said hydroformylation process is ethylene and said oxygenated product stream comprises propionaldehyde.

9. 9. A process in accordance with Claim 2 wherein said olefin converted in said hydroformylation process is a mixture of ethylene and propylene and said oxygenated product stream comprises a mixture of propionaldehyde and butyraldehyde.

10. 10. A process in accordance with Claim 1 wherein said olefin converted in said hydroformylation process is at least one butene and said oxygenated product stream comprises valeraldehydes.

11. 11. A process for purifying a feed gas employed in a chemical conversion process for the production of oxygenated compounds; wherein said feed gas comprises at least one of carbon monoxide and hydrogen; said process comprising intimately contacting said feed gas with at least a portion of the oxygenated product stream obtained from said chemical conversion process prior to introducing said feed gas into the chemical conversion reaction zone.

12. 12. A process in accordance with Claim 11 wherein said intimate contacting is a countercurrent contacting of liquid oxygenated product stream and feed gas.

13. 13. A process in accordance with Claim 12 wherein said countercurrent contacting is carried out at substantially the same pressure as is the pressure of said chemical conversion process.

14. 14. A process in accordance with Claim 11 wherein said contacting is carried out at a temperature in the range of about 25.degree. up to 100.degree.C.

15. 15. A process in accordance with Claim 14 wherein said contacting is carried out at a temperature in the range of about 40.degree. up to 65.degree.C.

16. 16. A process in accordance with Claim 11 wherein said chemical conversion process is a hydro.shy. formylation process.

17. 17. A process in accordance with Claim 16 wherein the starting material subjected to said hydroformylation process is an olefin having 2 up to 8 carbon atoms.

18. 18. A process in accordance with Claim 16 wherein the starting material subjected to said hydroformylation process is selected from the group consisting of:

- ethylene,
- propylene,
- butenes

as well as mixtures of any two or more thereof.

19. 19. A process in accordance with Claim 16 wherein said oxygenated product stream comprises butyraldehyde.

20. 20. A process in accordance with Claim 19 wherein said oxygenated product stream further comprises propionaldehyde.

21. 21. A process in accordance with Claim 20 wherein said oxygenated product stream further comprises valeraldehydes.

22. 22. A process in accordance with Claim 11 wherein said chemical conversion process a Fisher-Tropsch reaction.

23. 23. A process in accordance with Claim 11 wherein said chemical conversion process is an alcohol homologation reaction.

24. 24. A process in accordance with Claim 11 wherein said chemical conversion process is an anhydride-forming reaction.

GRANTED-PATENT

ACCESSION NUMBER: 325446 EUROPATFULL EW 199318 FS PS STA B
TITLE: Impurity removal from carbon monoxide and/or hydrogen-containing streams.
INVENTOR(S): Butler, Gerald Eugene c/o EASTMAN KODAK COMPANY, Patent Department 343 State Street, Rochester New York 14650, US
PATENT ASSIGNEE(S): EASTMAN KODAK COMPANY (a New Jersey corporation), 343 State Street, Rochester New York 14650, US
PATENT ASSIGNEE NO: 201210
AGENT: Phillips, Margaret Dawn et al, Kodak Limited Patent Department Headstone Drive, Harrow, Middlesex HA1 4TY, GB
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MAIN: C07C045-50
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DETDEN; CLMEN; CLMDE; CLMFR
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DESCRIPTION (ENGLISH):

This invention relates to the purification of gas feed streams comprising carbon monoxide and/or hydrogen. In a particular aspect, this invention relates to an integrated process wherein the reaction product stream is employed to purify the feed gases employed for a chemical conversion process.

Background of the Invention

Many chemical conversions are known which employ hydrogen and/or carbon monoxide-containing gases. These gases frequently contain small amounts of impurities which are detrimental to the desired chemical conversions. As a result, numerous treatments have been developed to remove such impurities such as oxygen, elemental sulfur, organic as well as inorganic sulfur compounds, iron, and the like. Each such impurity removal process introduces added requirements for equipment (e.g., scrubbers, guard beds, and the like), the maintenance thereof, utility consumption, and the like. It would be desirable to eliminate the need for such added equipment and materials as fixed beds containing alumina, zinc oxide, and the like.

Accordingly, a relatively simple, inexpensive means to remove undesirable impurities from carbon monoxide and/or hydrogen-containing feed streams would be of great benefit to numerous chemical conversion reactions.

EP-A-0 216 258 describes a process for the purification of a gas e.g. a synthesis gas containing hydrogen sulfide, hydrogen cyanide or carbonyl sulfide as an impurity. It comprises contacting the gas with at least one aliphatic aldehyde which is liquid under the conditions of purification.

Objects of the Invention

An object of the present invention, therefore, is a process for the removal of impurities from carbon monoxide and/or hydrogen-containing feed streams employed for chemical conversion reactions.

Another object of the present invention is a chemical conversion process employing carbon monoxide and/or hydrogen-containing gases wherein **deactivating** impurities are readily and inexpensively removed from the gaseous feed stream.

These and other objects of the present invention will become apparent upon inspection of the detailed description and appended claims which follow.

Statement of the Invention

In accordance with the present invention, I have discovered that the common impurities in carbon monoxide and/or hydrogen-containing feed streams, i.e., oxygen, sulfur, iron, and the like, can be removed by contacting such gas streams with the oxygenated product stream obtained from a process in which the carbon monoxide and/or hydrogen are fed as a co-reactant.

The practice of the present invention allows one to eliminate the need for ancillary gas purification equipment, such as a fixed bed purification column, thereby saving the capital and maintenance costs associated with such equipment. In addition, the invention process enables the efficient recovery and recycle of unreacted gaseous components from the product stream. Moreover, the invention process accomplishes the removal of many undesirable components from the carbon monoxide and/or hydrogen-containing feed streams, including water vapor.

In particular, the invention enables the removal of molecular oxygen from a gas feed comprising carbon monoxide and hydrogen which is used in a hydroformylation process employing a rhodium-phosphine catalyst so that phosphine loss is avoided.

In accordance with the present invention, there is provided a hydroformylation process wherein an olefin is contacted with a gas feed comprising carbon monoxide and hydrogen in the presence of a rhodium-phosphine catalyst to produce an **aldehyde**, characterized

in that the gas feed does not contain hydrogen sulfide, hydrogen cyanide or carbonyl sulfide as an impurity and is intimately contacted with at least a portion of the **aldehyde** product stream obtained from the hydroformylation process prior to feeding the gas to the hydroformylation zone whereby molecular oxygen present in the gas feed is removed therefrom.

Brief Description of the Figure

Figure 1 is a flow diagram of an exemplary scheme incorporating the process of the present invention.

Detailed Description of the Invention

The contacting of feed gas with oxygenated product stream in accordance with the present invention can be carried out under a variety of conditions. For example, the pressure of the contacting can vary from about 0.709MPa up to 4.053MPa (7 up to 40 atmospheres). Preferably, pressure of the contacting will be carried out at approximately the same pressure as is being employed for the chemical conversion process. In this way, unreacted feed components for the desired conversion can be stripped from the crude oxygenated product and recycled into the chemical conversion reaction without the need for recompression, cooling, condensation, or the like.

Similarly, the temperature at which the contacting is performed can vary widely, and will be a function of the pressure, the nature of the oxygenated product employed for the contacting, the length of time during which feed gas and oxygenated product are maintained in intimate contact, and the like. The lower temperature employed is determined by the efficiency of impurity removal desired (with contacting at too low a temperature being essentially ineffectual); while at excessively high contact temperatures, substantial quantities of liquid reaction product are stripped from Vessel 11 and returned to the reactor. In addition, excessively high temperatures cause an increased formation of by-products. Typically, temperatures in the range of about 25.degree. up to 100.degree.C are suitable for the contacting, with temperatures in the range of about 40.degree. up to 65.degree.C being preferred.

The contacting time and ratio of feed gas to liquid oxygenated reaction product can each vary widely. Generally, sufficient time of contact is maintained to allow a major proportion of the feed gas impurities to be absorbed by the liquid reaction product. Similarly most any ratio of feed gas to liquid is suitable, so long as the volume of liquid employed is sufficient to absorb a major proportion of the impurities contained in the feed gas.

Referring now to Figure 1, the invention will be described with particular reference to the apparatus illustrated therein. The flow of crude feed gases via Line 1 and recycled gases via Line 53 into Compressor 7 is controlled by Valve 3. The combined gas stream is subjected to compression up to the desired reaction pressure then passed through Line 9 into Vessel 11 in which the crude feed gas stream and a portion of reactor effluent are brought into intimate contact with one another.

As employed in this specification, the term "intimate contact" refers to any means by which the gas-liquid interface between crude feed gas and reactor effluent is maximized. Those of skill in the art recognize that this can be accomplished in a variety of ways. For example, the crude feed gas can be passed upwardly in a countercurrent fashion through a body of reactor effluent. Alternatively, crude feed gas can be sparged into a body of reactor effluent. The column dimensions can vary widely and are not believed to be critical. The presence of column packings may increase the efficiency of the contacting operation, as will certain column designs

which cause turbulent fluid flow through the column to occur.

Once crude feed gases and reaction product have been intimately contacted, the treated feed gas stream passes via Line 13 and is combined with organic feed stream (introduced via Line 17), with the combined feed streams being introduced into Reactor 19 (via Line 15). After having contacted crude feed gas in Vessel 11, crude oxygenated reaction product is removed from Vessel 11 via Line 45 where product is recycled to Vessel 11 via Pump 57 and Line 59 (in order to control the gas/liquid ratio), or product is controllably delivered to Flash Tank 51 via Valve 47 and Line 49. The gases obtained in the flash tank are recycled via Line 53 and admixed with additional crude feed gas being introduced via Line 1. The crude reaction product obtained from the crude reaction tank is removed via Line 55 and delivered to crude product tank for further manipulation.

Returning now to Reactor 19, reactor volume is maintained fairly constant by removing a vaporous stream overhead via Line 21. The vaporous reactor effluent is passed through Chiller 23 then into Vapor/Liquid Separator 27 via Line 25. Gaseous products are taken overhead via Line 29 and either recirculated to the reaction vessel via Line 33, Recirculator 35, Lines 37 and 15 or, as appropriate, overhead gases are removed from the reaction train via inert Purge Line 31. Liquid product is removed from Vapor/Liquid Separator 27 via Line 39. This material is then pumped via Pump 41 through Line 43 into Vessel 11 where the crude reaction product is contacted with additional quantities of crude feed gas.

As Figure 1 and the above description of the figure make clear, the oxygenated reaction product itself is used to remove undesirable impurities from the crude feed gas stream. At the same time, unreacted quantities of the organic reactant feed via Line 17 can be stripped from the crude product stream in Vessel 11 and returned directly to the reaction vessel (No. 19) without the need for recompression of such organic feed material.

A presently preferred application of the invention process is in the hydroformylation reaction wherein olefins having 2 up to 20 carbon atoms are converted to **aldehydes** having $n + 1$ carbon atoms. Preferred olefins are α -olefins having 2 up to 8 carbon atoms. Exemplary hydroformylation reactions include the conversion of propylene to n-butyraldehyde, ethylene to propionaldehyde, butenes to valeraldehydes, as well as conversions of mixed olefin feeds to produce mixed **aldehyde** products.

The invention will now be described in greater detail by reference to the following non-limiting examples.

Example 1: Effect of Temperature on Oxygen Removal

Example 1 shows how the process of the present invention can be employed to remove molecular oxygen from a crude synthesis gas stream using the product liquid of a hydroformylation reaction. A hydro-formylation reaction utilizing a rhodiumphosphine catalyst system to produce butyraldehydes was operated at a pressure of 1.824MPa (18 bars). The molecular oxygen scrubber employed was a 1.52.4mm (6-inch) diameter by 3.66m (12 foot) tall tower packed with 12.7mm (1/2-inch) stainless steel Pall rings. A ratio of product liquid to crude feed gas of $19.38 \times 10^3 \text{ min}^{-1} \cdot \text{sup}^3 \cdot \text{m}^{-3}$ (5.12 US gal.) of product liquid per standard cubic foot (std. ft.³) ($2.83 \times 10^3 \text{ min}^{-1} \cdot \text{sup}^2 \cdot \text{m}^3$) of feed gas was maintained, at a feed gas rate of about $14.7 \times 10^3 \text{ min}^{-1} \cdot \text{sup}^2 \cdot \text{m}^3 / \text{s}$ (187 std. ft.³/hour). When the average temperature of the molecular oxygen scrubber was about 40.degree.C, the average daily phosphine losses to phosphine oxide (caused by the presence of molecular oxygen in the feed gases) were 2.08 percent of the phosphine in the reactor. When the average temperature of the scrubber was increased to 55.degree.C, the

average daily phosphine losses to phosphine oxide were reduced to 1.3875 percent of the phosphine in the reactor, for a 34 percent reduction in phosphine losses.

Example 2: Effect of Pressure on Oxygen Removal

A 203.2mm (8-inch) diameter by 3.048m (10-foot) tall absorption tower filled with 19.05mm (3/4-inch) Intalox saddles was used to evaluate absorption of trace quantities of oxygen from a stream of nitrogen using crude butyraldehydes as absorption liquid. In the first test the pressure of the system was $10 \times 10^5 \text{ Pa}$ (1 bar). An oxygen meter was used to measure oxygen concentration in both the incoming and outgoing nitrogen stream. In the second and third tests the pressure was raised to $7 \times 10^5 \text{ Pa}$ (7 bar). The temperature for all three tests was 50-60.degree.C.

The results are shown in Table 1. <table> The results indicate that O_2 will be absorbed at both low pressure and high pressure but that oxygen absorption is more nearly complete at the higher pressure.

Example 3: Removal of Sulfur-Containing Impurities

A test was run to evaluate the removal of sulfur bearing lubricating oil from synthesis gas utilizing the scrubber described in Example 1. The lubricating oil contained 2,055 ppm sulfur. The addition of oil was at a rate such that the sulfur content in the reactor would increase by 26 ppm per day if all the sulfur entered the reactor. During the 6 days of oil addition, the sulfur content in the reactor was unchanged. These data indicate the scrubber utilizing product aldehydes as absorption liquid will stop sulfur bearing oil from entering the reactor.

Example 4: Removal of Iron-Containing Impurities

A test was run to evaluate removal of iron carbonyl from synthesis gas utilizing the scrubber described in Example 1. A solution of ironpentacarbonyl in butyraldehyde was added to the high pressure synthesis gas feed line between the compressor and the molecular oxygen scrubber. The scrubber temperature was 55.degree.C at the base. Scrubber pressure was about $19 \times 10^5 \text{ Pa}$ (19 bar). The iron containing solution was added continuously at a rate of about 0.04 gram of iron per hour for 72 hours. During this time a total of 0.024 gram iron accumulated in the reactor. This indicates that the scrubber removed 99.2 percent of the iron from the incoming synthesis gas.

Example 5: Recovery and Recycle of Unreacted Propylene From Crude Hydroformylation Product Stream

A test was run to evaluate desorption of low boilers from the crude product aldehydes using the apparatus described in Example 1. The crude product aldehydes were contacted at $14 \times 10^5 \text{ Pa}$ (14 bar) and 55.degree.C with incoming synthesis gas. The crude aldehydes collected in Vessel 51 were then reduced in pressure to $0.5 \times 10^5 \text{ Pa}$ (0.5 bar) and heated to 90.degree.C to force the dissolved low boilers to flash from the liquid to form a low pressure recycle stream.

In a comparison run, the crude product aldehydes were removed from the Reactor 19, passed directly to flash Chamber 27, then reduced in pressure from $14 \times 10^5 \text{ Pa}$ (14 bar) to $0.5 \times 10^5 \text{ Pa}$ (0.5 bar), and heated to 90.degree.C to force dissolved synthesis gas and propylene to flash from the crude product aldehydes. These flashed gases make up the low pressure recycle.

The results of these runs are summarized in Table 2. <table> From Table 2 it is seen that the volume of low pressure recycle is very

significantly reduced by contacting the crude product **aldehydes** with the incoming synthesis gas prior to letting down the pressure.

CLAIMS (ENGLISH):

1. A hydroformylation process wherein an olefin is contacted with a gas feed comprising carbon monoxide and hydrogen in the presence of a rhodiumphosphine catalyst to produce an **aldehyde**,

characterized in that the gas feed does not contain hydrogen sulfide, hydrogen cyanide or carbonyl sulfide as an impurity and is intimately contacted with at least a portion of the **aldehyde** product stream obtained from the hydroformylation process prior to feeding the gas to the hydroformylation zone whereby molecular oxygen present in the gas feed is removed therefrom.

2. A process in accordance with Claim 1 wherein said intimate contacting is a countercurrent contacting of liquid oxygenated product stream and gaseous carbon monoxide and hydrogen feed.

3. A process in accordance with Claim 2 wherein said countercurrent contacting is carried out at substantially the same pressure as is the hydroformylation process.

4. A process in accordance with Claim 1 wherein said contacting is carried out at a temperature in the range of about 25.degree. up to 100.degree.C.

5. A process in accordance with Claim 4 wherein said contacting is carried out at a temperature in the range of about 40.degree. up to 65.degree.C.

6. A process in accordance with Claim 1 wherein said olefin converted in said hydroformylation process has in the range of 2 up to 8 carbon atoms.

7. A process in accordance with Claim 2 wherein said olefin converted in said hydroformylation process is propylene and said oxygenated product stream comprises butyraldehyde.

8. A process in accordance with Claim 2 wherein said olefin converted in said hydroformylation process is ethylene and said oxygenated product stream comprises propionaldehyde.

9. A process in accordance with Claim 2 wherein said olefin converted in said hydroformylation process is a mixture of ethylene and propylene and said oxygenated product stream comprises a mixture of propionaldehyde and butyraldehyde.

10. A process in accordance with Claim 1 wherein said olefin converted in said hydroformylation process is at least one butene and said oxygenated product stream comprises valeraldehydes.

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